



## *Supplement of*

# **Isotopic evidence for biogenic molecular hydrogen production in the Atlantic Ocean**

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**Due to the experimental upset and timing the following assumption have been made:**

- The glass vessel is initially under vacuum.
- The water sample flows into the glass vessel, equilibrates with the headspace and mix completely with the injected makeup gas.
- No significant exchange between the headspace / makeup gas mixture and the water phase will happen until the sample has been extracted into an evacuated flask.

**The following abbreviations and definitions have been used:**

- $V_h$ : volume headspace in the glass vessel (1.6 dm<sup>3</sup>)
- $V_w$ : volume water in the glass vessel (8.4 dm<sup>3</sup>)
- $V_t$ : volume gas transfer system (0.025 dm<sup>3</sup>)
- $V_f$ : volume flask and drying tube (1.1 dm<sup>3</sup>)
- $p_h$ : pressure headspace after transfer from Niskin bottle to glass vessel
- $p_{ht}$ : pressure headspace and gas transfer system before addition of makeup gas
- $p_{htm}$ : pressure headspace and gas transfer system after addition of makeup gas
- $p_f$ : pressure headspace, gas transfer system and flask after expansion to flask
- $c_{w0}$ : initial H<sub>2</sub> concentration in seawater
- $c_h$ : H<sub>2</sub> concentration in headspace after transfer from Niskin bottle to glass vessel
- $c_w$ : H<sub>2</sub> concentration in seawater after transfer from Niskin bottle to glass vessel
- $y_h$ : H<sub>2</sub> wet mole fraction in headspace after transfer from Niskin bottle to glass vessel
- $y_m$ : H<sub>2</sub> dry mole fraction makeup gas
- $y_{htm}$ : H<sub>2</sub> wet mole fraction in headspace and gas transfer system after addition of makeup gas
- $y_f$ : H<sub>2</sub> dry mole fraction sample flask
- $R$ : ideal gas constant (= 8.31446621 J K<sup>-1</sup> mol<sup>-1</sup>)
- $T$ : ambient absolute temperature (assumed to be equal to the gas temperature)

Defining the **extraction efficiency  $\eta$**  as

$$\eta = \frac{c_h V_h}{c_{w0} V_w} \quad (1)$$

the **initial concentration of H<sub>2</sub> in seawater,  $c_{w0}$** , can be calculated from

$$c_{w0} = \frac{c_h V_h}{\eta V_w} \quad (2)$$

The concentration in the headspace,  $c_h$ , was not measured directly, but can be derived from the measured H<sub>2</sub> mole fraction in the sampling flask. The sampling procedure following gas extraction under vacuum can be broken into three steps (see Methods section):

1. Expansion of headspace
2. Addition of makeup gas
3. Expansion of headspace/makeup gas mixture into sampling flask

**Step 1:** The volume of the headspace increases from  $V_h$  to  $V_h + V_t$ , where  $V_t$  is the volume of the gas transfer system. The total pressure drops from  $p_h$  to  $p_{ht} = p_h V_h / (V_h + V_t)$ .  $H_2$  mole fraction,  $y_h$ , and isotope delta,  $\delta_h$ , do not change.

**Step 2:** Adding makeup gas changes the total pressure from  $p_{ht}$  to  $p_{htm}$ .  $H_2$  mole fraction and isotope delta also change. The  $H_2$  mole fraction after mixing with makeup gas is:

$$y_{htm} = (y_h - y_m) \frac{p_{ht}}{p_{htm}} + y_m \quad (3)$$

The initial headspace  $H_2$  concentration is calculated using the ideal gas law:

$$\begin{aligned} c_h &= \frac{y_h p_h}{RT} = \frac{p_h}{RT} \left[ (y_{htm} - y_m) \frac{p_{htm}}{p_{ht}} + y_m \right] \\ &= \frac{1}{RT} \left[ (y_{htm} - y_m) p_{htm} \left( 1 + \frac{V_t}{V_h} \right) + y_m p_h \right] \end{aligned} \quad (4)$$

**Step 3:** The gas is expanded from the manifold into a sampling flask, passing through a drying trap. At this stage the mole fractions are changed due to drying of the gas. The volume of the system also changes, but this affects the  $H_2O$  and  $H_2$  mole fractions by the same ratio.

Thus,  $y_{htm}$  is calculated from the measured dry mole fraction in the flask,  $y_f$ , as

$$y_{htm} = y_f \left[ 1 - \frac{p_h(H_2O)}{p_{htm}} \frac{V_h}{V_h + V_t} \right] \quad (5)$$

where  $p_h(H_2O)$  is the initial water vapour pressure in the headspace. Due to the short time periods involved ( $< 4$  min), water vapour equilibration is assumed not to occur upon subsequent pressure changes in the system.

Combining equations (2), (4) and (5), the initial seawater concentration can be calculated as

$$\begin{aligned} c_{w0} &= \frac{(y_{htm} - y_m)(V_h + V_t)p_{htm} + y_m V_h p_h}{\eta V_w RT} \\ &= \frac{y_f \left[ \left( 1 + \frac{V_t}{V_h} \right) p_{htm} - p_h(H_2O) \right] - y_m \left[ \left( 1 + \frac{V_t}{V_h} \right) p_{htm} - p_h \right]}{\eta V_w RT} \end{aligned} \quad (6)$$

$y_f$ ,  $y_m$ ,  $p_{htm}$ ,  $V_t$ ,  $V_h$  and  $V_w$  were measured.  $R$  is a constant ( $= 8.31446621 \text{ J K}^{-1} \text{ mol}^{-1}$ ).

$T$  is the ambient lab temperature and assumed to be equal to the gas and water temperature. Since ambient lab temperature and surface water temperature were never more than  $1.2^\circ \text{C}$  apart, this assumption is unlikely to cause an error of more than  $0.4\%$  in  $c_{w0}$ .

$p_h(H_2O)$  was assumed to be equal to the equilibrium vapour pressure (calculated following Green and Carritt (1967)) of seawater at temperature  $T$  and at its actual salinity, which was measured to within  $0.01 \text{ g kg}^{-1}$ .

The extraction efficiency,  $\eta$  can be calculated from the following mass balance

$$V_w c_{w0} = V_h c_h + \alpha V_w c_h \quad (7)$$

Assuming that headspace and water phase are in equilibrium, the ratio of the H<sub>2</sub> concentration in water and in the headspace is given by the Ostwald coefficient

$$\alpha = \frac{c_w}{c_h} \quad (8)$$

This gives for the initial concentration in the water

$$c_{w0} = \left( \frac{V_h}{V_w} + \alpha \right) c_h \quad (9)$$

and for the extraction efficiency as defined in equation (2)

$$\eta = \left( 1 + \alpha \frac{V_w}{V_h} \right)^{-1} \quad (10)$$

In the present case,  $\alpha = \alpha(\text{H}_2)$  was equal to  $0.0163 \pm 0.0001$ , which gives  $\eta = 92\%$  for  $V_w/V_h = 8.4/1.6 = 5.25$ .

$p_h$  was not measured and had to be estimated from the gas concentrations in the water.

$$\begin{aligned} p_h &= p_h(\text{N}_2) + p_h(\text{O}_2) + p_h(\text{Ar}) + p_h(\text{CO}_2) + p_h(\text{H}_2\text{O}) \\ &= RT \left[ c_h(\text{N}_2) + c_h(\text{O}_2) + c_h(\text{Ar}) + c_h(\text{CO}_2) \right] + p_h(\text{H}_2\text{O}) \\ &= RT \left[ \frac{c_{w0}(\text{N}_2)}{\frac{V_h}{V_w} + \alpha(\text{N}_2)} + \frac{c_{w0}(\text{O}_2)}{\frac{V_h}{V_w} + \alpha(\text{O}_2)} + \frac{c_{w0}(\text{Ar})}{\frac{V_h}{V_w} + \alpha(\text{Ar})} + \frac{c_{w0}(\text{CO}_2)}{\alpha(\text{CO}_2)} \right] + p_h(\text{H}_2\text{O}) \end{aligned} \quad (11)$$

The extraction efficiencies of all gases were assumed to follow their solubilities. Due to the buffering effect of the CO<sub>2</sub> system (CO<sub>2</sub>(w), H<sub>2</sub>CO<sub>3</sub>, HCO<sub>3</sub><sup>-</sup> and CO<sub>3</sub><sup>2-</sup>), the dissolved CO<sub>2</sub> concentration changes by only 1 or 2 % during extraction, so that the headspace concentration can be estimated from  $c_{w0}(\text{CO}_2)/\alpha(\text{CO}_2)$ .

$p_h$  was estimated to vary between 98 and 111 hPa, with contributions of 46 to 52 hPa from N<sub>2</sub>, 23 to 27 hPa from O<sub>2</sub>, 1.1 to 1.3 hPa from Ar, 0.4 hPa from CO<sub>2</sub> and 17 to 40 hPa from H<sub>2</sub>O.

Based on equation (4), the **isotope delta of the headspace gas** can be calculated as follows

$$\delta_h = \frac{\delta_{\text{htm}} y_{\text{htm}} \left( 1 + \frac{V_t}{V_h} \right) p_{\text{htm}} - \delta_m y_m \left[ \left( 1 + \frac{V_t}{V_h} \right) p_{\text{htm}} - p_h \right]}{y_{\text{htm}} \left( 1 + \frac{V_t}{V_h} \right) p_{\text{htm}} - y_m \left[ \left( 1 + \frac{V_t}{V_h} \right) p_{\text{htm}} - p_h \right]} \quad (12)$$

Two alternative scenarios were considered to derive the initial isotope delta of dissolved H<sub>2</sub>, with scenario 1 assuming equilibrium isotopic fractionation between headspace and water, and scenario 2 assuming kinetic isotopic fractionation during extraction from Niskin bottle to glass vessel.

**Scenario 1:** Correction of  $\delta_h$  for equilibrium isotopic fractionation between headspace and water

The equilibrium isotope fractionation between water and headspace is defined as

$$\varepsilon = \frac{1 + \delta_w}{1 + \delta_h} - 1 \quad (13)$$

The isotopic mass balance equation between headspace and water can then be described via

$$V_w c_{w0} \delta_{w0} = V_h c_h \delta_h + V_w c_w \delta_w \quad (14)$$

which gives for the isotope delta of the original dissolved gas:

$$\delta_{w0} = \frac{\varepsilon(1 + \delta_h)}{1 + \frac{V_h}{V_w} \frac{1}{\alpha}} + \delta_h \quad (15)$$

The equilibrium isotope fractionation between dissolved phase and gas phase is  $\varepsilon = (37 \pm 1) \%$  at 20 °C (Knox et al., 1992). The temperature dependence of  $\varepsilon$  is unknown and was neglected here.

**Scenario 2:** Correction for kinetic isotopic fractionation between headspace and water

If kinetic isotope fractionation applies, then the isotopic composition of the residual gas in the water is

$$\delta_w = (1 + \delta_{w0}) \left( \frac{c_w}{c_{w0}} \right)^{\varepsilon_k} - 1 = (1 + \delta_{w0}) (1 - \eta)^{\varepsilon_k} - 1 \quad (16)$$

Then, the isotope delta of the accumulated gas in the headspace is

$$\delta_h = (1 + \delta_{w0}) \frac{1 - (1 - \eta)^{1 + \varepsilon_k}}{\eta} - 1 \quad (17)$$

which gives for the isotope delta of the original dissolved gas:

$$\delta_{w0} = \frac{(1 + \delta_h) \eta}{1 - (1 - \eta)^{1 + \varepsilon_k}} - 1 \quad (18)$$

The kinetic isotope fractionation during gas evasion is  $\varepsilon_k = (-18 \pm 2) \%$  at 20 °C (Knox et al., 1992). The temperature dependence of  $\varepsilon_k$  is unknown and was neglected here.

## References:

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